

Silicon electro-optic switches using microring resonators with phase-tunable feedback

Linjie Zhou and Andrew W. Poon

Department of Electrical and Electronic Engineering, The Hong Kong University of Science and Technology,
Clear Water Bay, Hong Kong SAR, China

Tel: (852)-2358-7905; Fax: (852)-2358-1485; Email: eeawpoon@ust.hk

Abstract: We report a silicon electro-optic switch using a microring resonator with phase-tunable feedback. We show a wide mode spacing of four-times the ring free-spectral range. The carrier-induced blue-shifted resonance maintains a high extinction ratio.

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OCIS codes: (230.5750) Resonators; (230.2090) Electro-optical devices

Silicon electro-optic switches and modulators [1, 2] using free-carrier plasma effect [3] have been attracting considerable recent interest. In order to enhance the device sensitivity to the small carrier-induced refractive index changes, Xu et al. [2] demonstrated a promising approach using high-Q microring resonators that are laterally integrated with p-i-n diodes and thereby causing resonance shifts upon biasing the diode. However, one shortcoming is that the blue-shifted resonance exhibits a significantly reduced extinction ratio due to the phase mismatch between the carrier-injected ring microresonator and the coupled passive waveguide.

In this summary, we report our initial experimental demonstration of an alternative way to electro-optically tune the silicon microresonator resonances by means of a phase-tunable feedback. The key merits are that the phase-control is enabled in a feedback-waveguide external to the microresonator, and thus the resonance wavelengths and extinction ratios can be tuned while preserving the waveguide-microresonator phase matching.

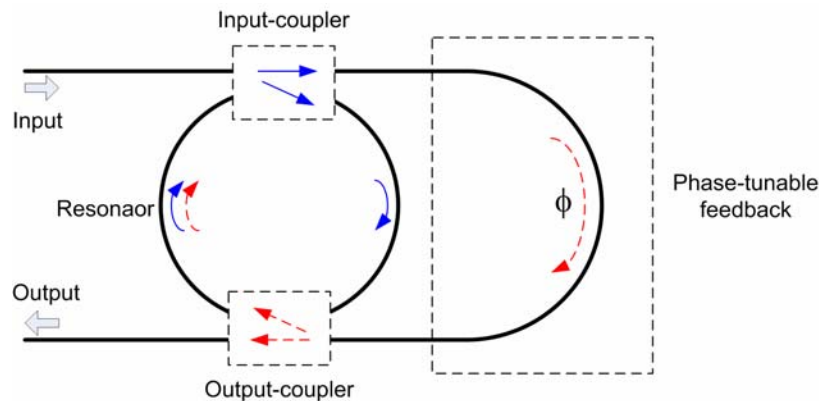


Fig.1. Schematic of the electro-optic switch comprising a microring resonator that is input- and output-coupled to a bended waveguide providing phase-tunable feedback. ϕ : electro-optically tunable feedback phase.

Figure 1 shows the schematic illustration of the optical switch using a microring resonator input- and output-coupled to a bended waveguide. The waveguide provides a phase-tunable external feedback to the microring resonator. Here we outline the device principle. The input light wave is first split by the input-coupler, coupling part of the light wave to the resonator, and part of the light wave to the feedback-waveguide, as depicted by

the solid arrows. The feedback-waveguide light wave accumulates a phase shift of ϕ upon reaching the output-coupler and partially couples back to the microring resonator, as depicted by the dashed arrows. The microring lightwave and the external feedback lightwave can then interfere. Thus, by electro-optically tuning ϕ using a forward-biased p-i-n diode, we can obtain controlled resonance tuning without directly tuning the resonator.

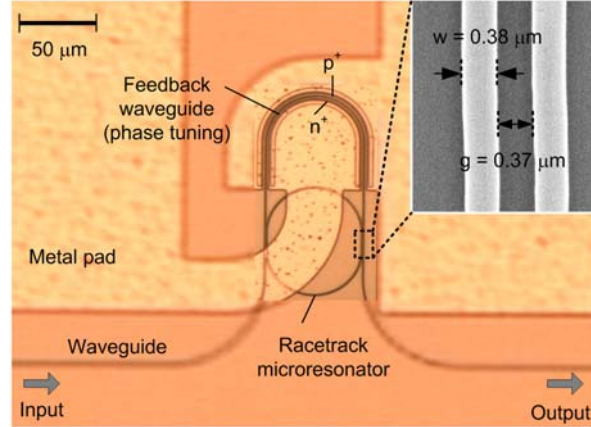


Fig.2. (a) Optical micrograph of our fabricated silicon electro-optic switch using a racetrack ring microresonator input- and output-coupled to a Ω -shaped single-mode waveguide. A lateral p-i-n diode is integrated along the U-bend of the feedback waveguide for phase tuning. Inset: scanning electron micrograph of the microresonator-waveguide coupling region before the oxide cladding deposition.

We fabricated our devices on a silicon-on-insulator wafer with a $0.21\ \mu\text{m}$ device layer and a $2\text{-}\mu\text{m}$ buried oxide layer. We employed i-line ($365\ \text{nm}$) photolithography and RIE dry etching. We implanted $1 \times 10^{20}\ \text{cm}^{-3}$ phosphorous dopants for the n^+ region and 2×10^{19} boron dopants for the p^+ region. The entire device is clad with a $0.6\text{-}\mu\text{m}$ -thick low temperature oxide layer for electrical isolation and a $0.7\text{-}\mu\text{m}$ -thick patterned aluminum layer for electrical connections. Figure 2 shows the top-view optical micrograph of our fabricated device. The device comprises a racetrack ring microresonator that is input- and output-coupled to a single-mode Ω -shaped waveguide. The racetrack ring comprises $25\text{-}\mu\text{m}$ -radius curved waveguides joined with $10\text{-}\mu\text{m}$ -long straight waveguides. A $130\text{-}\mu\text{m}$ -long p-i-n diode is laterally integrated with the feedback waveguide. The diode comprises heavily-doped $4\text{-}\mu\text{m}$ -wide n^+ and p^+ regions located in the slab layer outside the ridge waveguide, with a separation of $\sim 0.5\ \mu\text{m}$ from the waveguide sidewalls in order to minimize the mode-field overlap with the absorptive doped regions. The inset shows the scanning electron micrograph of the coupling region (before the oxide cladding deposition). The measured waveguide width is $\sim 0.38\ \mu\text{m}$ and the gap size is $\sim 0.37\ \mu\text{m}$.

Figures 3(a) and 3(b) show the measured TE-polarized (electric field // device plane) transmission spectra of our device and a control notch filter (a straight waveguide coupled with a racetrack ring microresonator) in order to contrast our device performance with that of a conventional notch filter. We discern only 3 pronounced resonances (denoted as A, B and C) in the wavelength range of $1540\ \text{nm} - 1560\ \text{nm}$ for our device. Resonance B ($\sim 1544.4\ \text{nm}$) has the highest Q of $\sim 10^4$ and the largest extinction ratio of $\sim 18\ \text{dB}$. The absence of pronounced resonances between resonances B and C indicates a mode spacing of $\sim 13\ \text{nm}$. In comparison, the conventional notch filter exhibits single-mode resonances with a Q-factor of $\sim 5,600$, an extinction ratio of $< 8\ \text{dB}$, and a free-spectral range (FSR) of $3.36\ \text{nm}$ (nearly 4 times less than the mode spacing of our device). We attribute the wide mode spacing and the large extinction ratio observed from our device to the wavelength-dependent ϕ that determines the resonance coupling strength between the feedback-waveguide and microresonator.

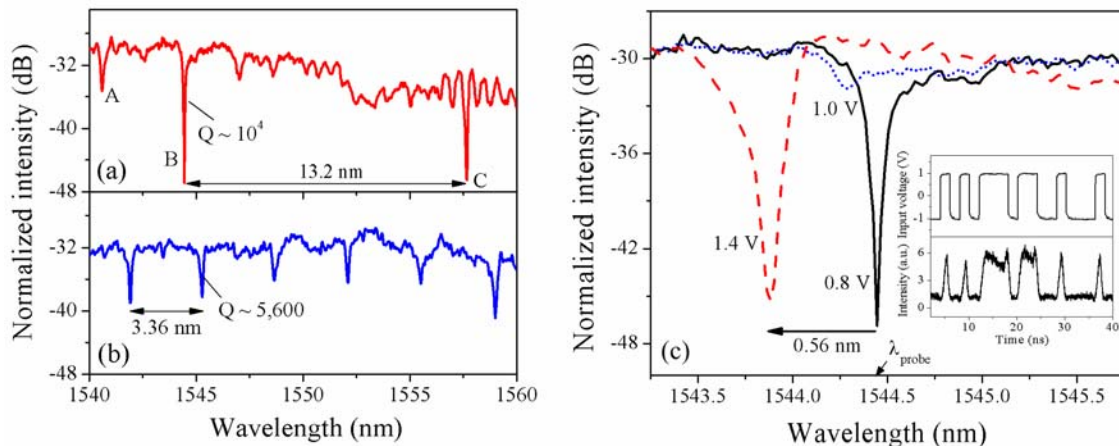


Fig.3. Measured TE-polarized transmission spectra for (a) our device without biasing the p-i-n diode, and (b) a conventional notch filter. (c) Electro-optical tuning of the resonance around 1544 nm under various DC bias voltages of $V_d = 0.8$ V (solid line), 1.0 V (dotted line), and 1.4 V (dashed line). Inset: modulated 0.5 Gbit/s NRZ optical waveform under ± 1 V electrical signal at probe wavelength of ~ 1544.4 nm.

Figure 3(c) shows the measured resonance B transmission spectra under various DC forward biases from 0.8 V to 1.4 V across the p-i-n diode. The spectrum upon 0.8-V forward bias (current 0.016 mA) is nearly identical to the spectrum upon zero bias. Upon a 1-V forward bias (current ~ 0.86 mA), the resonance is blueshifted (due to the free-carrier plasma dispersion [3]) and substantially suppressed. We attribute this resonance suppression upon a small increment in driving voltage to a nearly total destructive interference between the feedback and microresonator lightwaves. As the bias voltage exceeds 1.0 V, the resonance reappears and further blueshifts. Under 1.4 V forward bias (current 5.97 mA), the resonance extinction ratio (~ 15 dB) nearly recovers to the maximum level (zero bias) with a total resonance wavelength blueshift of ~ 0.56 nm. The Q-factor is reduced to $\sim 4,000$, mainly due to the free-carrier absorption loss.

We also modulate our device (at resonance B) using a non-return-to-zero (NRZ) electrical signal (± 1 V amplitude and 0.5 Gbit/s). The inset of Fig. 3(c) shows the modulated optical waveform and the driving signal, revealing that our device modulation speed can be up to 0.5 Gbit/s with the waveform suffering only slight distortions. The device bandwidth can be optimized by, say, reducing the free-carrier transition times in the p-i-n diode.

In summary, we experimentally demonstrated a silicon electro-optic switch using a racetrack microring resonator with phase-tunable feedback enabled by an integrated lateral p-i-n diode. We measured a resonance mode spacing of about 4 times wider than the ring microresonator free-spectral range. By applying forward-bias voltages on the order of 1 V across the p-i-n diode, we demonstrated resonance tuning with controlled extinction ratio, with up to about ~ 15 dB extinction ratio at a ~ 0.5 nm blueshifted resonance.

References

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